

## DESIGN OF REINFORCED CONCRETE SLAB

### Flexural Reinforcement (ACI 318-95)

\*adapted from CSI SAFE(TM) Design Manual

Data:

Thickness,  
 $h := 6.0 \text{ in}$

Depth of tensile reinf.,  
 $d_c := 1 \text{ in}$

Effective depth,  
 $d := 5 \text{ in}$

Depth of comp. reinf.,  
 $d' := 1 \text{ in}$

Concrete strength,  
 $f'_c := 4.0 \text{ ksi}$

Yield strength of steel,  
 $f_y := 60.0 \text{ ksi}$

Elasticity modulus of steel,  
 $E_s := 29000 \text{ ksi}$

Strength reduction factor,  
 $\phi_b := 0.90$

Strip width,  
 $b := 12.0 \text{ in}$

Minimum steel reinforcement,

$$A_{s;\min} := 0.0018 \cdot b \cdot h \cdot \frac{60000 \text{ psi}}{f_y}$$

$$A_{s;\min} = 0.1296 \text{ in}^2$$

Concrete stress block factors,

$$\beta_{1;\text{calc}} := 0.85 - 0.05 \cdot \left( \frac{f'_c - 4000 \text{ psi}}{1000 \text{ psi}} \right)$$

$$\beta_{1;\text{calc}} = 0.85$$

$$\beta_1 := \begin{cases} \text{if } \beta_{1;\text{calc}} < 0.65 \\ 0.65 \\ \text{else} \\ \text{if } \beta_{1;\text{calc}} > 0.85 \\ 0.85 \\ \text{else} \\ \beta_{1;\text{calc}} \end{cases}$$

$$\beta_1 = 0.85$$

Neutral axis depth at balanced,

$$c_b := \frac{87000 \text{ psi}}{87000 \text{ psi} + f_y} \cdot d$$

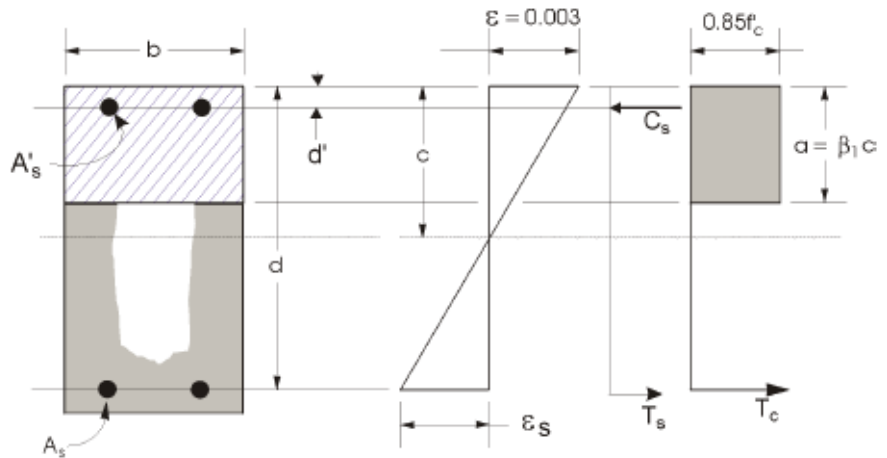
$$c_b = 2.959 \text{ in}$$

$$a_{\max} := 0.75 \cdot \beta_1 \cdot c_b$$

$$a_{\max} = 1.886 \text{ in}$$

Bending moment,

$$M_u := 317.952 \text{ kip in}$$



Depth of the compression block,

$$a := d - \sqrt{d^2 - \frac{2 \cdot |M_u|}{0.85 \cdot f'_c \cdot \phi_b \cdot b}} \quad a = 2.2283 \text{ in}$$

+

msg= "CASE(1) a > a\_max, Doubly Reinforcemenet"

+

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CASE(2) a > a\_max

Compressive force developed in concrete alone,

$$C := 0.85 \cdot f'_c \cdot b \cdot a_{\max} \quad C = 76.968 \text{ kip}$$

Moment resisted by concrete compression and tensile steel,

$$M_{uc} := C \cdot \left( d - \frac{a_{\max}}{2} \right) \cdot \phi_b \quad M_{uc} = 281.018 \text{ kip in}$$

$$M_{us} := M_u - M_{uc} \quad M_{us} = 36.934 \text{ kip in}$$

Stress in the compression steel,

$$f'_{s;calc} := 0.003 \cdot E_s \cdot \left( \frac{\frac{a_{\max} - d'}{\beta_1}}{\frac{a_{\max}}{\beta_1}} \right) \quad f'_{s;calc} = 47.8 \text{ ksi}$$

$$f'_s := \begin{cases} \text{if } f'_{s;calc} \leq f_y \\ f'_{s;calc} \\ \text{else} \\ f_y \end{cases} \quad f'_s = 47.8 \text{ ksi}$$

Area of required compression steel,

$$A_{s1} := \frac{M_{uc}}{f'_s \cdot \left( d - \frac{a_{\max}}{2} \right) \cdot \phi_b} \quad A_{s1} = 1.2828 \text{ in}^2$$

Tensile steel for balancing the compression in steel,

$$A_{s2} := \frac{M_{us}}{f_y \cdot (d - d') \cdot \phi_b} \quad A_{s2} = 0.171 \text{ in}^2$$

Total area of tensile steel,

$$A_s := A_{s1} + A_{s2} \quad A_s = 1.4538 \text{ in}^2$$